

CALCULATION, SIMULATION AND APPLICATION OF COMMERCIAL AND LIGHT INDUSTRIAL CO₂ HEAT PUMPS

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refrigerants delivered by mother nature

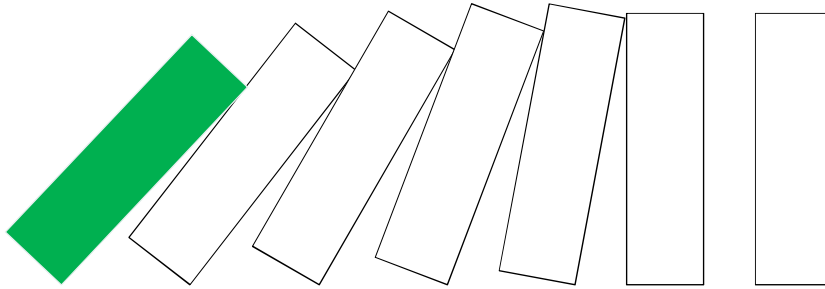
CALCULATION, SIMULATION AND APPLICATION OF COMMERCIAL AND LIGHT INDUSTRIAL CO₂ HEAT PUMPS

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- Introduction and Boundary Conditions
- Results of the work
- Summary and Conclusions

MOTIVATION

Heating and Cooling with Natural Refrigerants – a Way to Decarbonization. The present work is based on an air to water heat pump with CO₂ as refrigerant. In the form of a short analytical study, an attempt is made to identify possible influences that could result from the use of a more efficient compressor in an otherwise unchanged system.



HEAT PUMP APPLICATIONS WITH CO₂ AS REFRIGERANT

Hot or tap water heat pumps with CO₂ as refrigerant are predestined for applications with low water inlet -, high water outlet temperatures and high hot water demand, e.g. for bath loving people in spas and hotels, or in industrial applications.

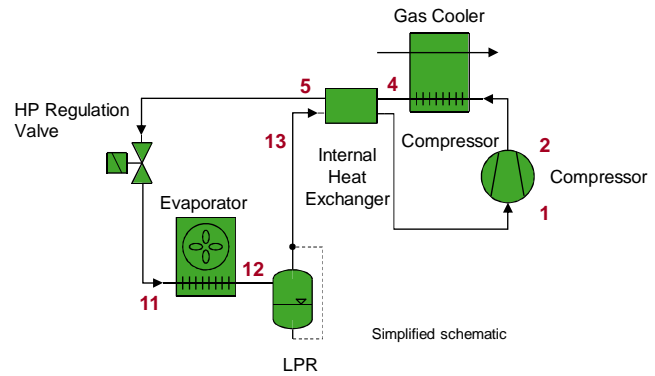
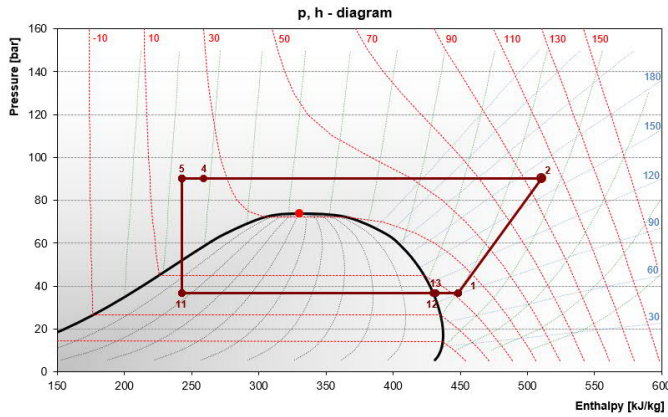
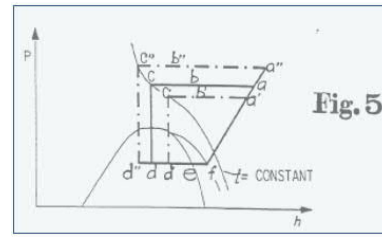
Influences on COP:

- Heat source (air, waste water, etc.)
- Heat source temperature range to decide for monovalent, bivalent design
- Evaporator design
- Control on refrigeration circuit and water side
- Water storage tank and stratification
- Gas cooler design
- Oil return
- Choice of lubricant
- Defrost operation

HEAT PUMP APPLICATIONS WITH CO₂ AS REFRIGERANT

Gustav-Lorentzen-Cycle

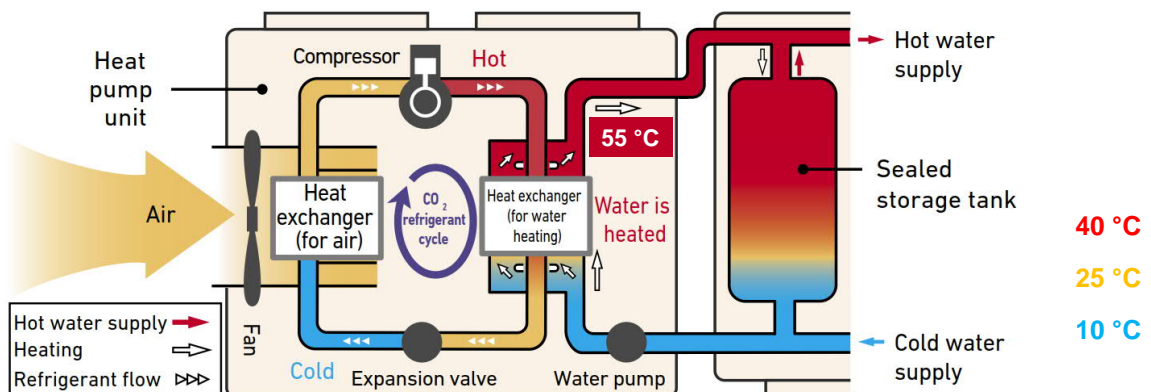
- Single stage compression and expansion
- Control of optimum discharge pressure
- No control of superheat – evaporator operates semi-flooded
- Low pressure receiver and internal heat exchanger required



Schematic shows the so-called Gustav-Lorentzen-Cycle

HEAT PUMP APPLICATIONS WITH CO₂ AS REFRIGERANT

- Basic operating modes are charging, re-heating and tapping mode
- Process of water heating is transient
- This work is based on a reference temperature of 55 °C for the water outlet
- Considered water inlet temperatures are 10 °C (start heating), 25 °C and 40 °C (end heating, or re-heating)



BOUNDARY CONDITIONS

Internal heat exchanger (IHX):

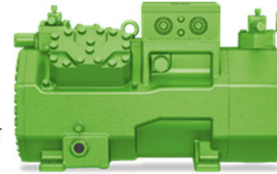
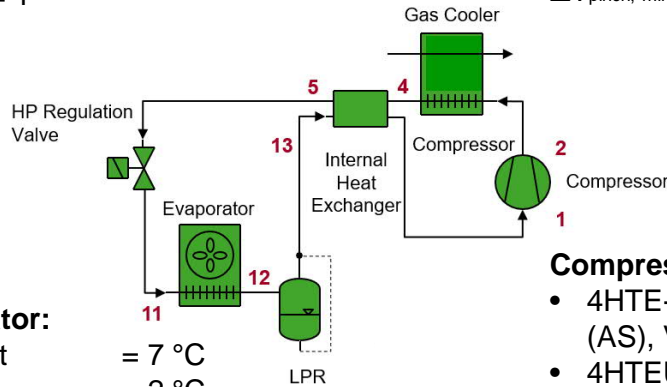
$T_{oh, min}$ (start value) ≈ 7 K, then T_{oh} f(m_r , ΔT_m)
 $A = 0,46$ m²
 No. of plates = 22
 Water passes = 1

Gas cooler:

$P_{HP} = 80; 85; 90; 95; 100; 120$ bara
 $t_{water\ inlet} = 10; 25; 40$ °C
 $t_{water\ outlet} = 55$ °C
 $\Delta T_{pinch, min} = 3$ K*

Evaporator:

$t_{ambient} = 7$ °C
 $t_o = 2$ °C
 $T_{oh, evaporator} = 0$ K



ADVANCED MOTOR TECHNOLOGY

Compressor: ECOLINE (TE) vs. ECOLINE+ (TE+)

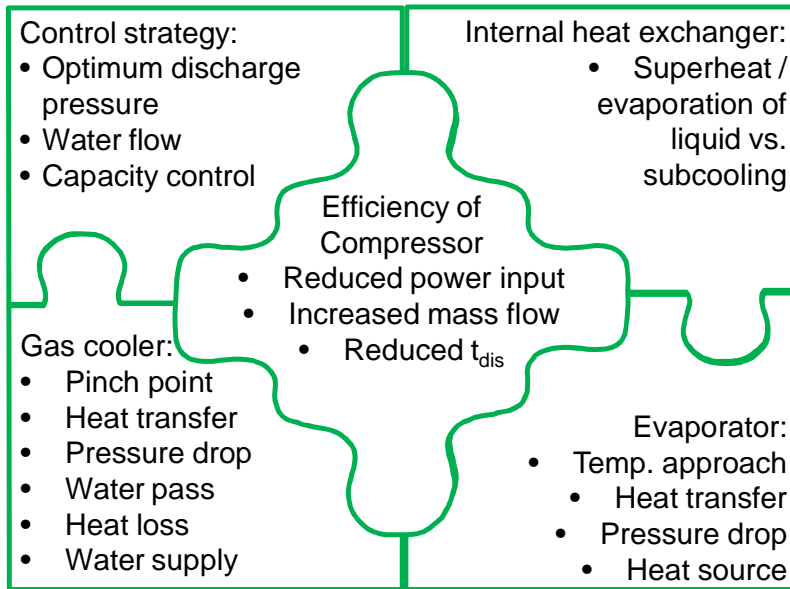
- 4HTE-20Z (TE) with standard asynchronous motor (AS), $V_{geo} = 12$ m³/h @ 1450 rpm
- 4HTEU-20LZ (TE+) with Line Start Permanent Magnet motor (LSPM), $V_{geo} = 12,4$ m³/h @ 1500 rpm
- Drive gear, including valve plates, equal

COMPRESSORS WITH LSPM MOTOR

Compressors with LSPM motors offer a higher COP. Increased efficiency is based on:

- Higher motor efficiency
- Higher mass flow rates due to synchronous speed
- Higher mass flow rates due to higher suction gas density \Rightarrow lower superheat across motor

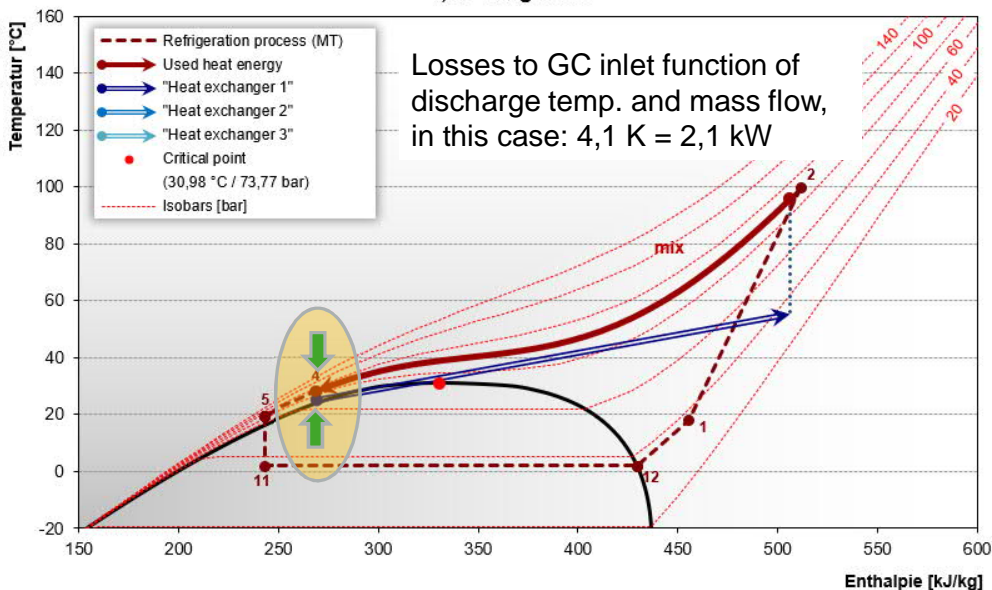
MAIN INFLUENCES ON COP_{HEATING}



PINCH POINT AND HEAT LOSS

- Visualisation of gas cooling heat transfer in t, h – diagram

t, h - Diagramm



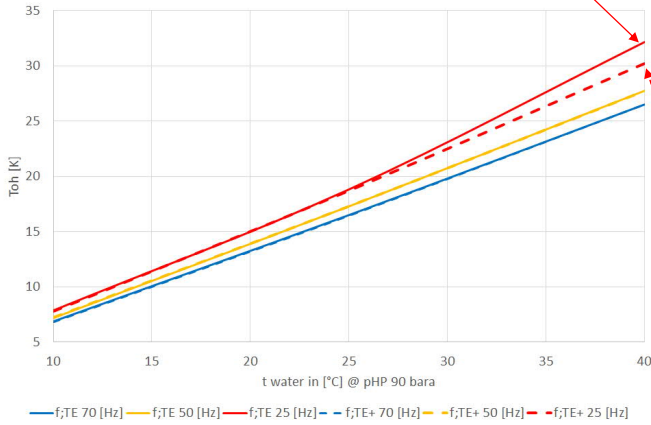
CO₂: 80 bara, t 85->28°C:
 t_{water} 25->55°C
 $\Delta T_{pinch} = -2,6 K$
 $\Delta T_{water in} = 3,1 K$
 $\Delta T_m = 4,9 K$

CO₂: 90 bara, t 96->28°C:
 t_{water} 25->55°C
 $\Delta T_{pinch} = \Delta T_{water in} = 3,0 K$
 $\Delta T_m = 11,4 K$

Pinch Point

RESULTS: INTERNAL HEAT EXCHAENGER

TE: $m_r / t_{dis} / Toh = 352 \text{ kg/h} / 131,1 \text{ }^\circ\text{C} / 32,2 \text{ K}$



TE+: $m_r / t_{dis} / Toh = 380 \text{ kg/h} / 124,5 \text{ }^\circ\text{C} / 30,1 \text{ K}$

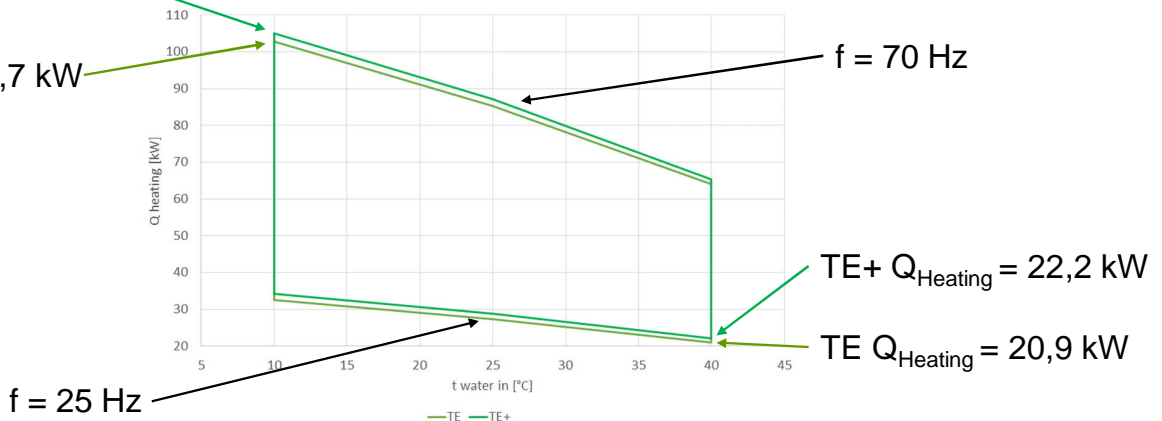
- Superheat is a function of water inlet temperature and compressor speed
- Significant difference in superheat between TE and TE+ compressor especially at high water inlet temperature and low operating frequency
- With increasing torque demand (p_o/p_{HP}), the difference between the rotational speed of an LSPM and AS motor becomes more significant ($f_{operating}$ 25 Hz 750 vs. < 725 rpm)
- The relative slip of the motor increases when the speed is reduced and thus losses and heating of the motor increase as well

RESULTS: CAPACITY MAPS

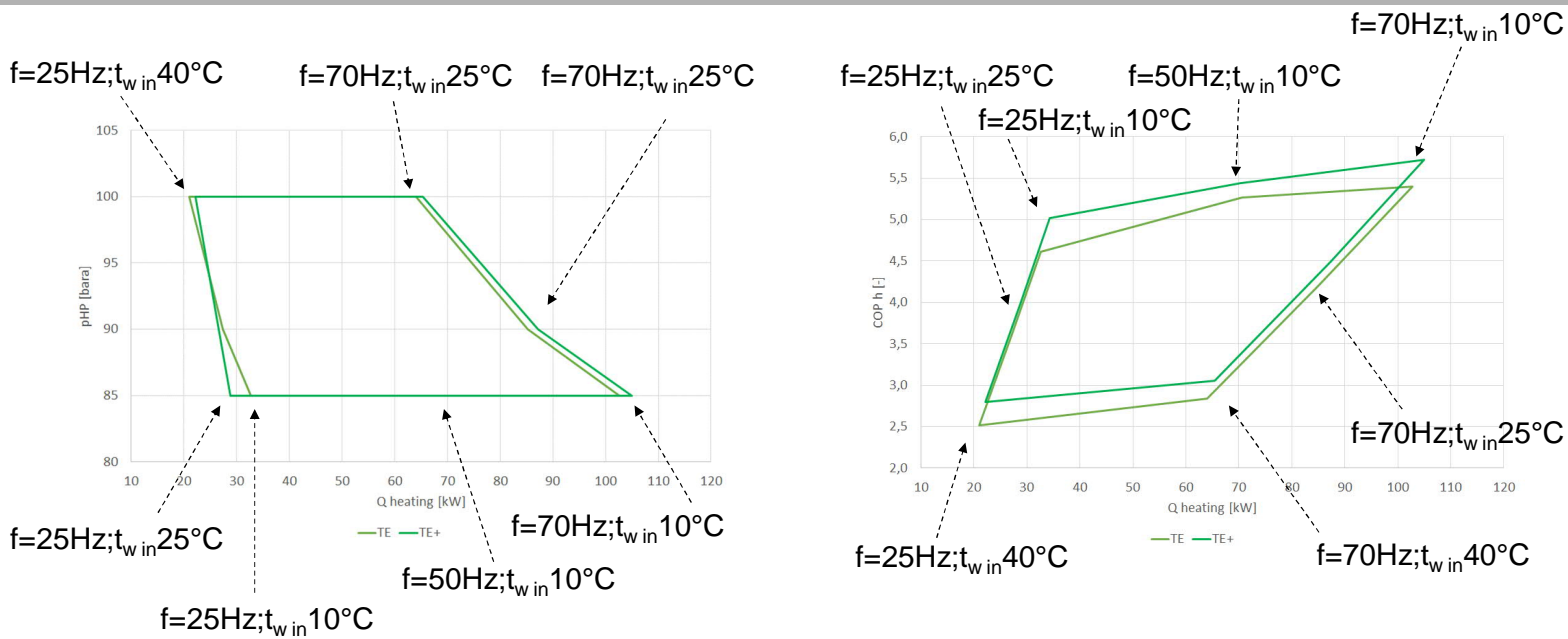
- Nominal capacity @ $t_{amb} / t_o / p_{HP} / f / t_{water\ inlet} / t_{water\ outlet} = 7 \text{ }^\circ\text{C} / 2 \text{ }^\circ\text{C} / 85 \text{ bara} / 70 \text{ Hz} / 10 \text{ }^\circ\text{C} / 55 \text{ }^\circ\text{C}$
- Minimum capacity @ $t_{amb} / t_o / p_{HP} / f / t_{water\ inlet} / t_{water\ outlet} = 7 \text{ }^\circ\text{C} / 2 \text{ }^\circ\text{C} / 100 \text{ bara} / 25 \text{ Hz} / 40 \text{ }^\circ\text{C} / 55 \text{ }^\circ\text{C}$

TE+ $Q_{Heating} = 105,3 \text{ kW}$

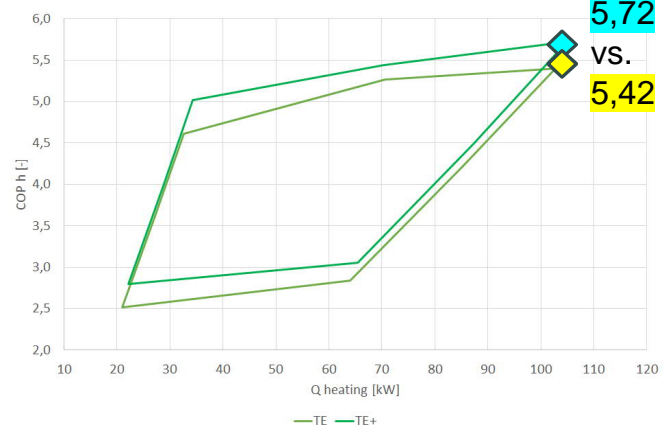
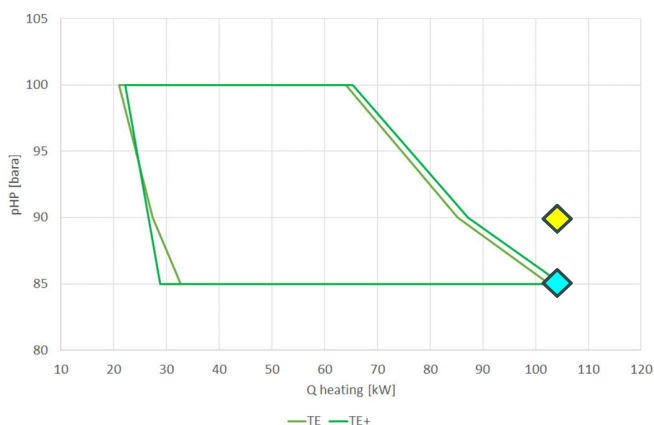
TE $Q_{Heating} = 102,7 \text{ kW}$



RESULTS: HIGH PRESSURE AND EFFICIENCY MAPS

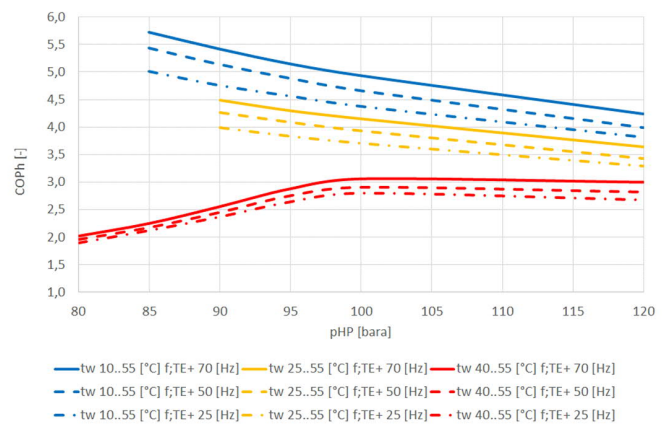
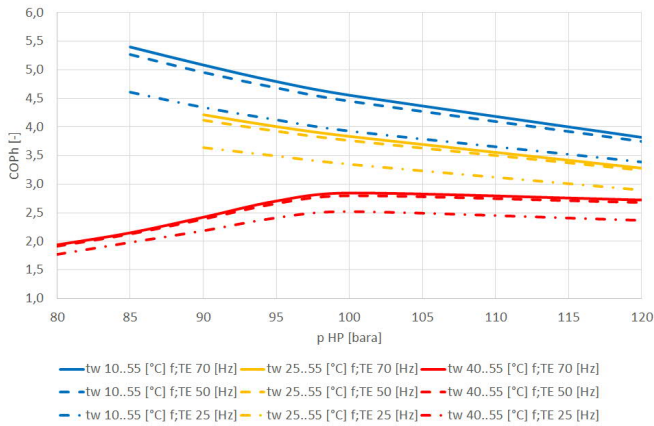


RESULTS: HIGH PRESSURE AND EFFICIENCY MAPS

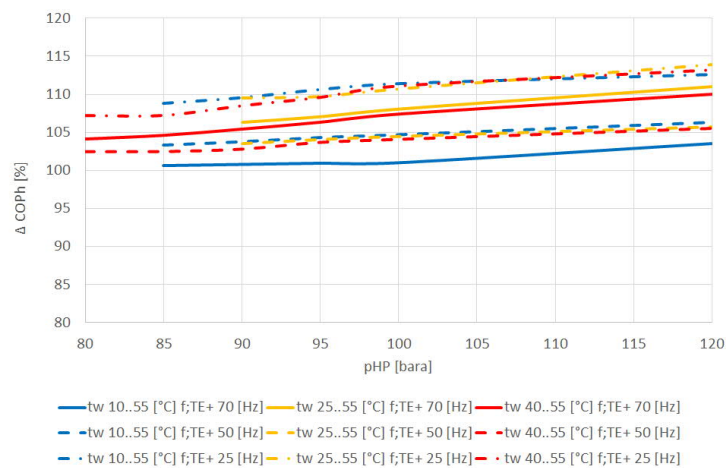


- ΔT_{pinch} @ 85 bara, 70 Hz, t_{water in} 10 °C: TE 3,0 K / TE+ 2,8 K
- ΔT_{pinch} @ 90 bara, 70 Hz, t_{water in} 10 °C: in both cases 3,0 K
- At this operating point, the influence of increased pressure for the heating capacity is low, but significant for efficiency. For the TE+ series, the disadvantage would be in the range of -5.5 percent.

RESULTS: COP AS FUNCTION OF DISCHARGE PRESSURE, WATER INLET TEMPERATURE AND FREQUENCY

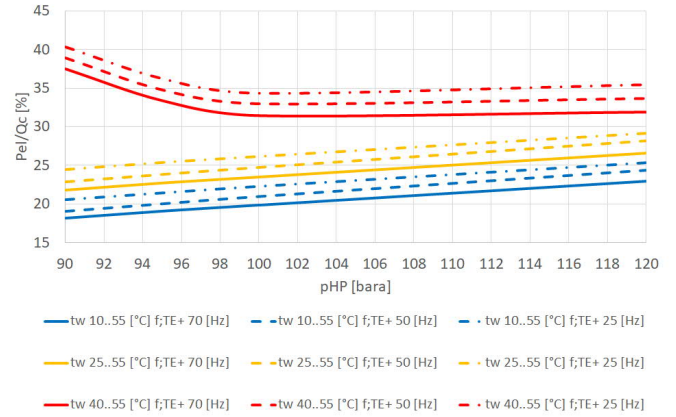
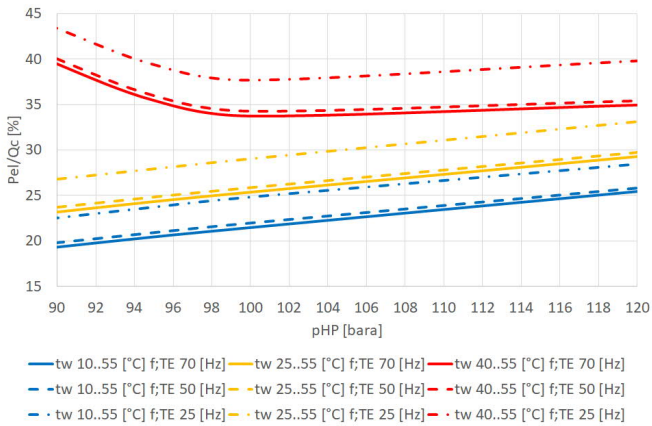


RESULTS: COP AS FUNCTION OF DISCHARGE PRESSURE, WATER INLET TEMPERATURE AND FREQUENCY

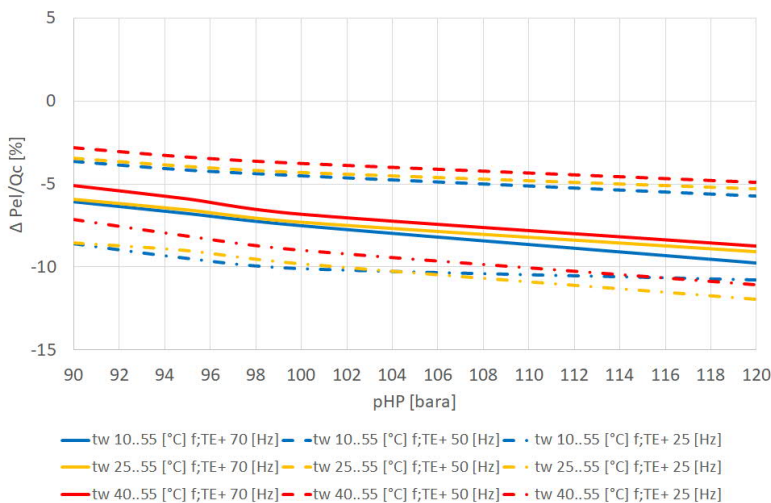


- $t_{\text{water inlet}}$ 10 and 25 °C : Highest COP with min ΔT_{pinch} and pHP
- $t_{\text{water inlet}}$ 40 °C : Highest COP with approx. 100 bar
- TE+: Highest increase in COP with 25 Hz and highest pressure ratio

RESULTS: SHARE OF POWER CONSUMPTION



RESULTS: SHARE OF POWER CONSUMPTION



- TE+: Share of power consumption in heat capacity is reduced
 - Share reduced with increasing pressure ratio
 - Most significant with 25 Hz operating frequency
 - Lowest change with 50 Hz
- Increased mass flow and potentially higher cooling capacity shows the basis for higher heating capacity of the unit with the TE+ compressor

SUMMARY & CONCLUSIONS – USING A MORE EFFICIENT COMPRESSOR WITH LSPM MOTOR IN AN OTHERWISE UNCHANGED SYSTEM

Within the scope of this work, a more efficient compressor with LSPM motor offers:

- Benefit in COP_h , especially with 25 Hz operating frequency of the compressor
- Increased heating capacity

However, it is important to note, that:

- The share of power consumption in the heat capacity decreases
- The level of discharge gas temperatures decreases as well
- The increase in heat output is achieved by an increase in mass flow and thus in cooling capacity
- The pinch point temperature difference is affected in a negative way with 10 and 25 °C water inlet temperature and discharge pressures < 90 bara

For the conditions considered:

- The trend of the optimum high pressures are the same
- A significant difference in superheat is generated by the IHX, especially at 40 °C water inlet temperature and 25 Hz operating frequency

THANK YOU FOR YOUR ATTENTION!

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